








## Forum 1: Planning and building

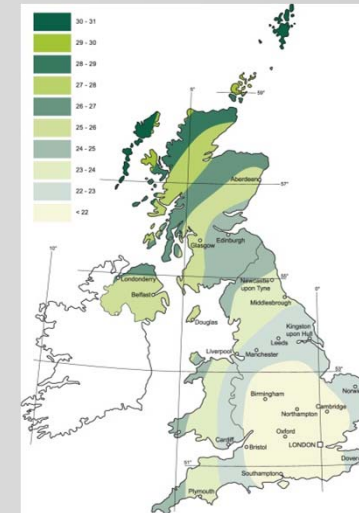
**Mounting and substructure and their importance for the power plant?**



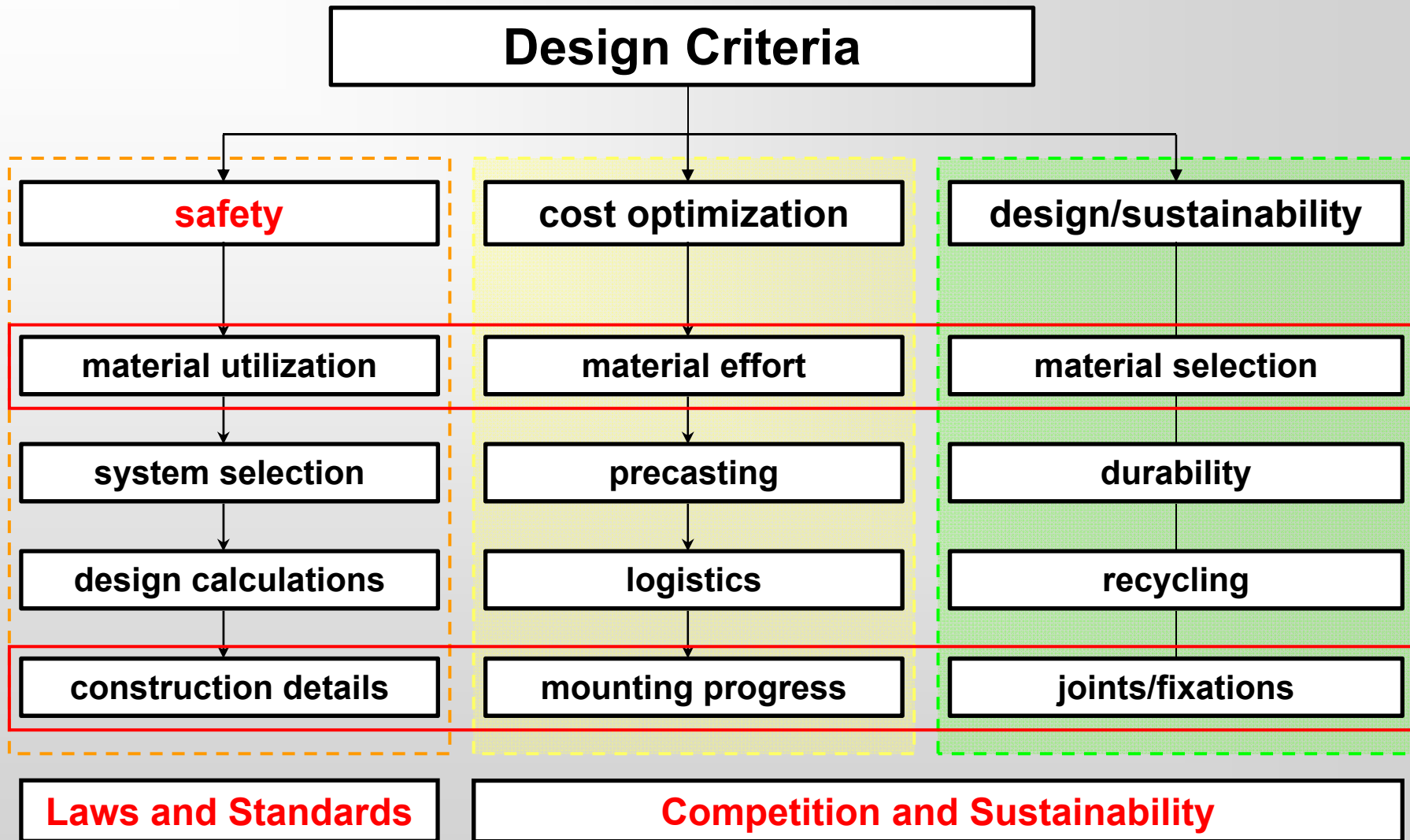
**10<sup>TH</sup>/11<sup>TH</sup> March, Paris, France**

## Overview of topics:

-  1. Introduction
-  2. Load evaluation
-  3. Design calculations
-  4. Decision criteria for a substructure selection
-  5. Foundation concepts
-  6. Mounting progress of foundation concepts
-  7. Summary

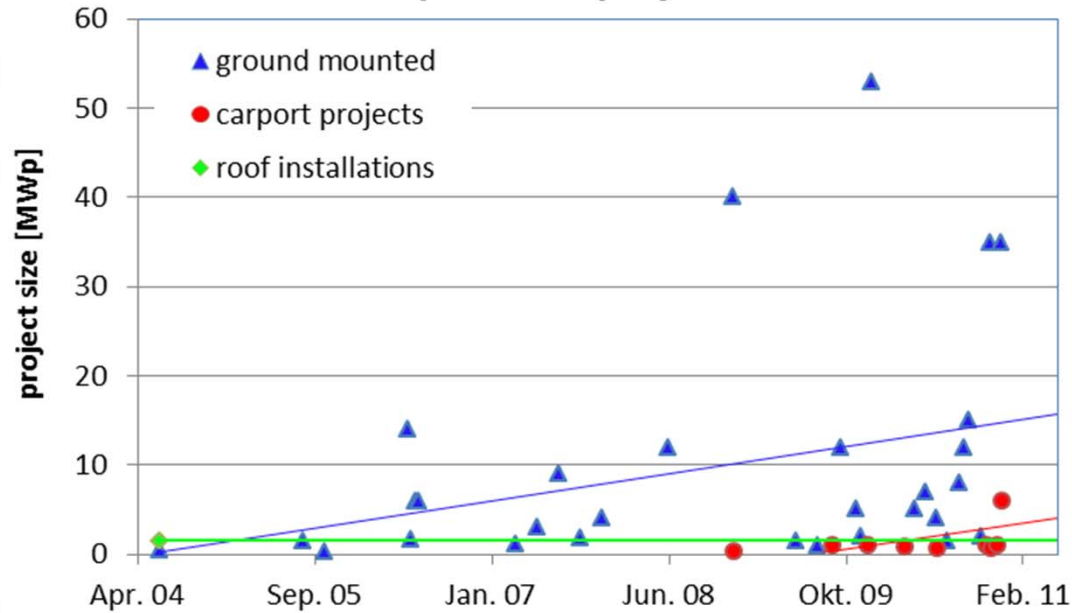


# 1. Introduction



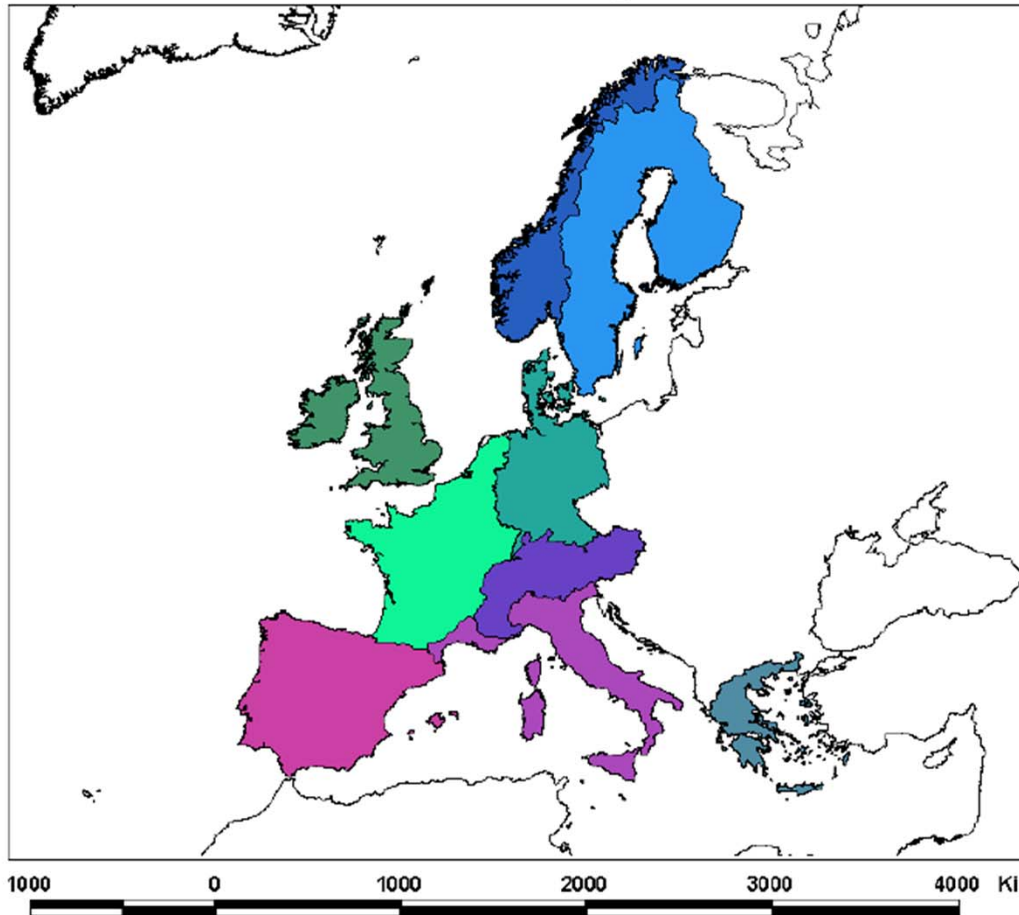
# Types of PV-Powerplants

development of project sizes



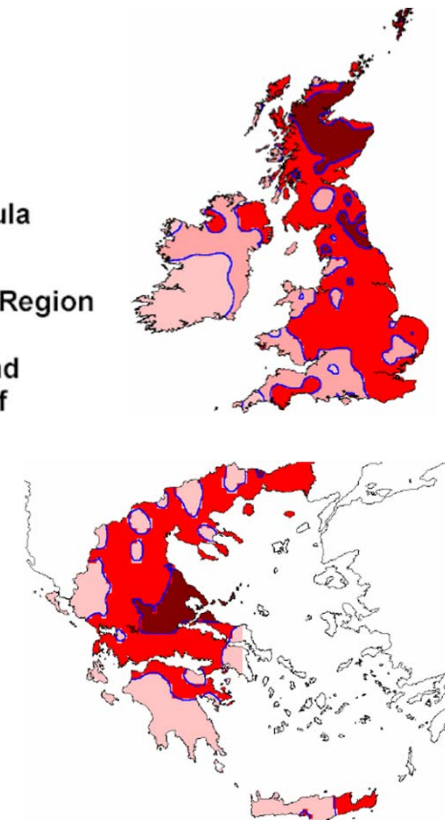
## 2. load actions

### Climatic Regions



Guidelines provided by EU  
Implementation by individual  
member states

- Alpine Region
- Central East
- Central West
- Greece
- Iberian Peninsula
- Mediterranean Region
- Norway
- Sweden, Finland
- UK, Republic of Ireland

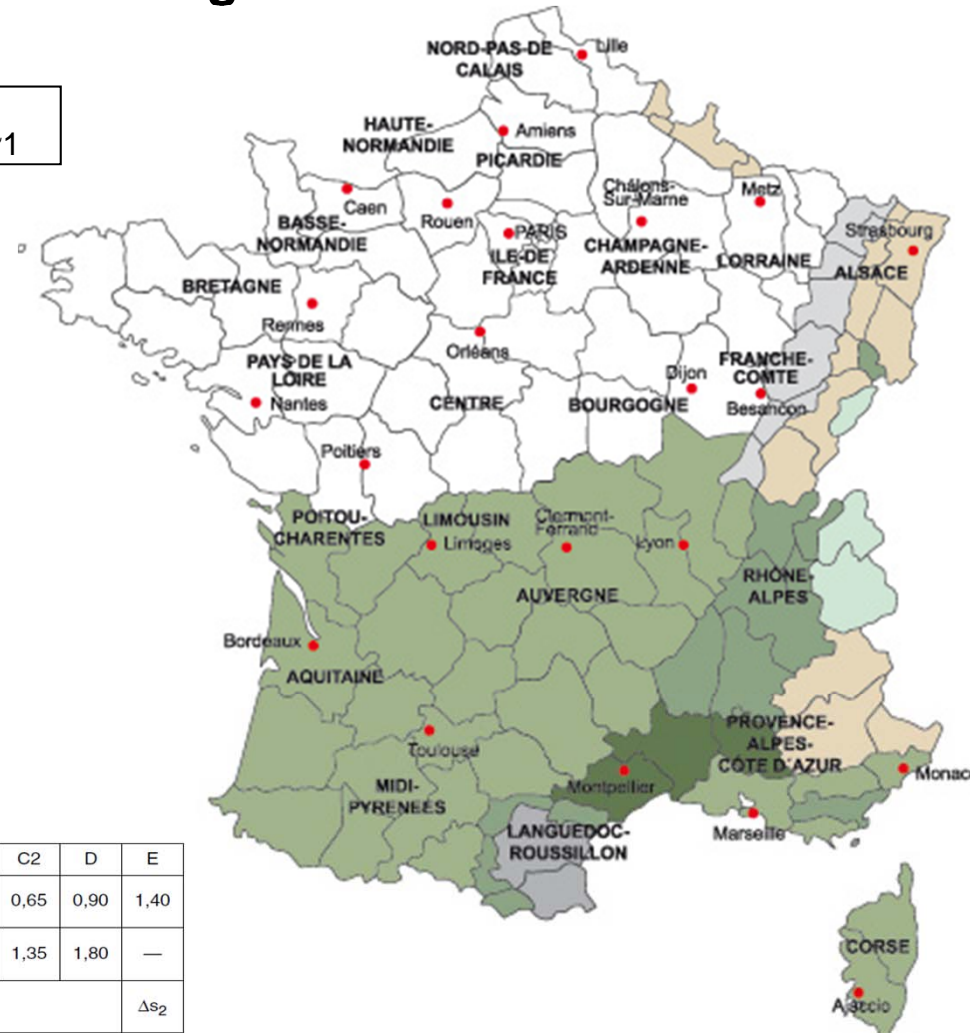
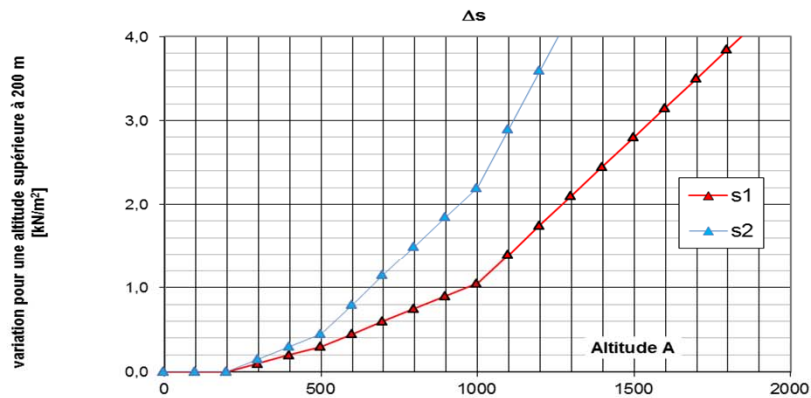
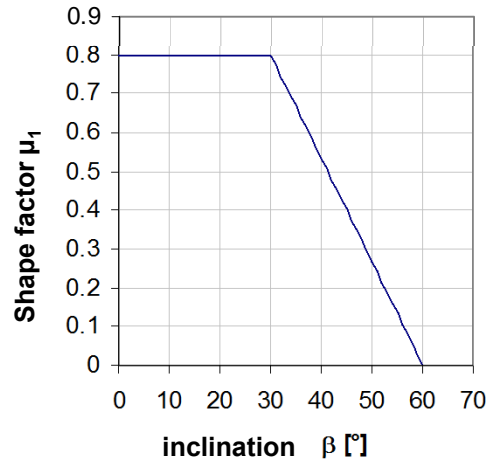


Example: International system for snow load evaluation



## Snow loads on the ground

$$s = (s_k + \Delta s) \cdot \mu_1$$



Régions :	A1	A2	B1	B2	C1	C2	D	E
Valeur caractéristique ( $S_k$ ) de la charge de neige sur le sol à une altitude inférieure à 200 m :	0,45	0,45	0,55	0,55	0,65	0,65	0,90	1,40
Valeur de calcul ( $S_{Ad}$ ) de la charge exceptionnelle de neige sur le sol :	—	1,00	1,00	1,35	—	1,35	1,80	—
Loi de variation de la charge caractéristique pour une altitude supérieure à 200 m :	$\Delta s_1$						$\Delta s_2$	

# European wind zone map according to Eurocode 1



**Basis:**

**Measurements (188 in D)**

**10-minutes median in  
10 m height above ground  
that occurs once every 50  
years**

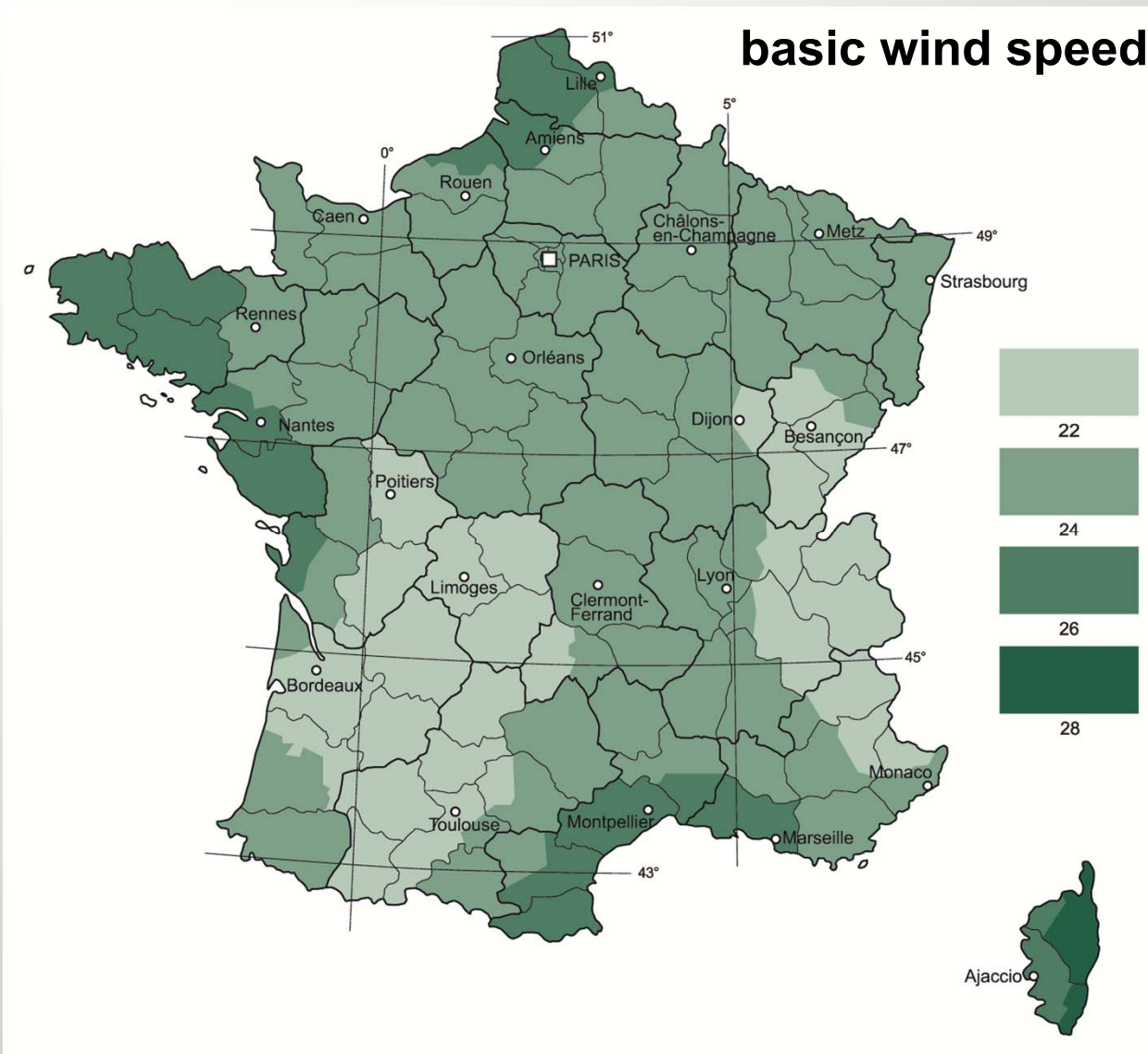
**observation period: 40-  
107 years**

**contains no gusts**

**applicable for flat, even  
terrain**



# France NF EN 1991-1-4/NA March 2008

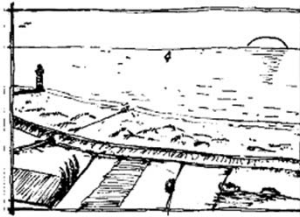




# Terrain categories according to Eurocode 1

## Terrain category 0

Sea, coastal area exposed to the open sea



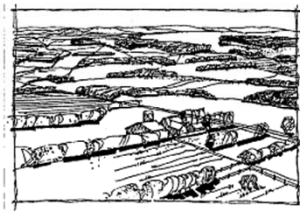
## Terrain category I (II in France)

Lakes or area with negligible vegetation and without obstacles



## Terrain category II (III a in France)

Area with low vegetation such as grass and isolated obstacles (trees, buildings) with separations of at least 20 obstacle heights



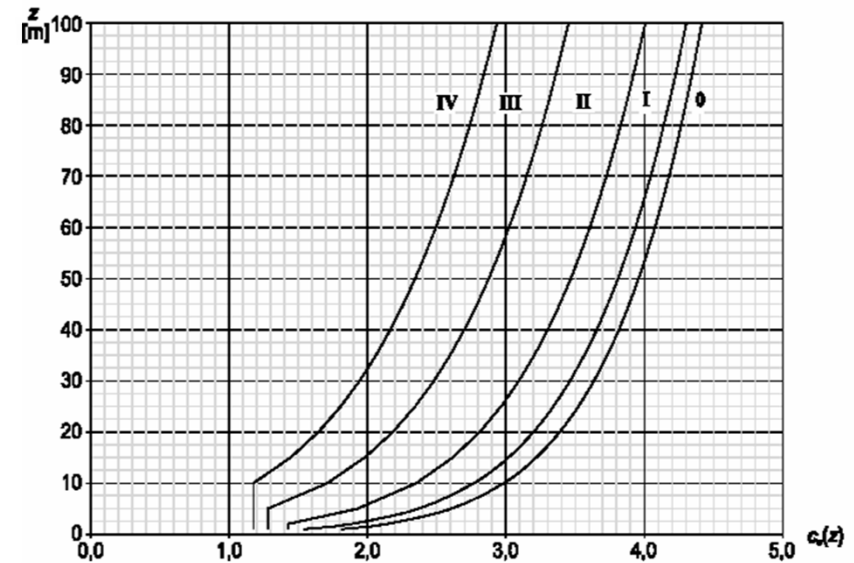
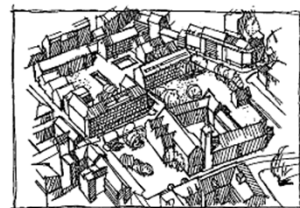
## Terrain category III (III b in France)

Area with regular cover of vegetation or buildings or with isolated obstacles with separations of maximum 20 obstacle heights (such as villages, suburban terrain, permanent forest)



## Terrain category IV

Area in which at least 15 % of the surface is covered with buildings and their average height exceeds 15 m



**Basis:**

$$q_b = \frac{1}{2} \cdot \rho \cdot v^2 \quad (\text{basic pressure})$$

$$\rho \quad \text{weight of air (1,25 kg/m}^2\text{)}$$

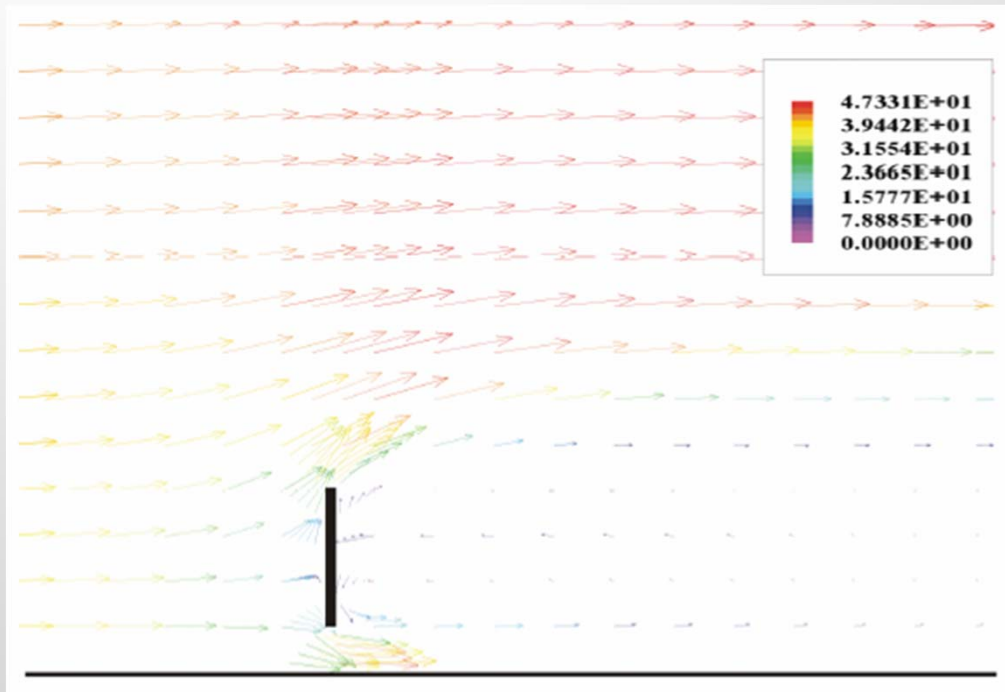
**Peak velocity pressure**

$$q_b(z) = C_e(z) \cdot q_b$$

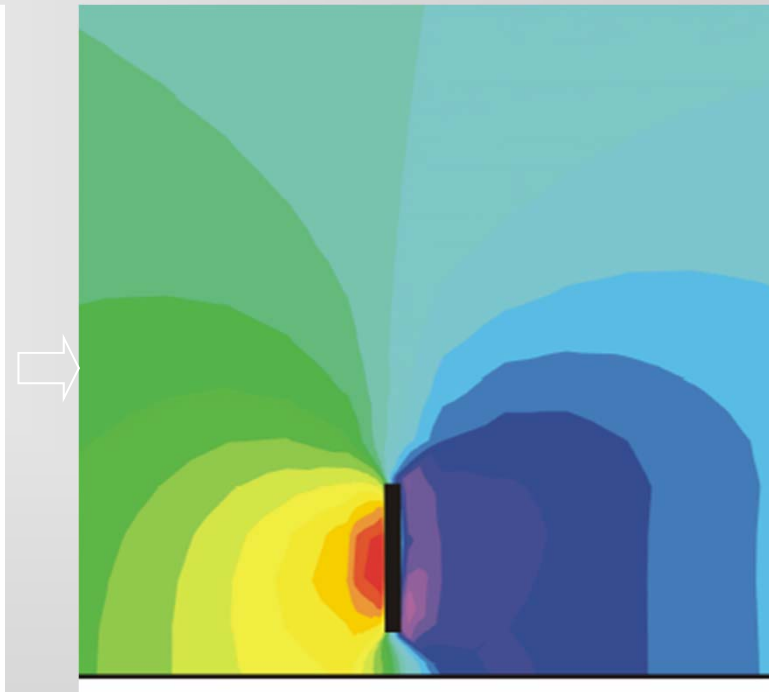
# Aerodynamic characteristics

## Pressure field if a vertical flow impacts the screen

Strömungsgeschwindigkeiten



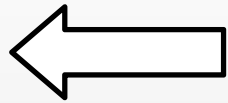
Pressure field (qualitative)



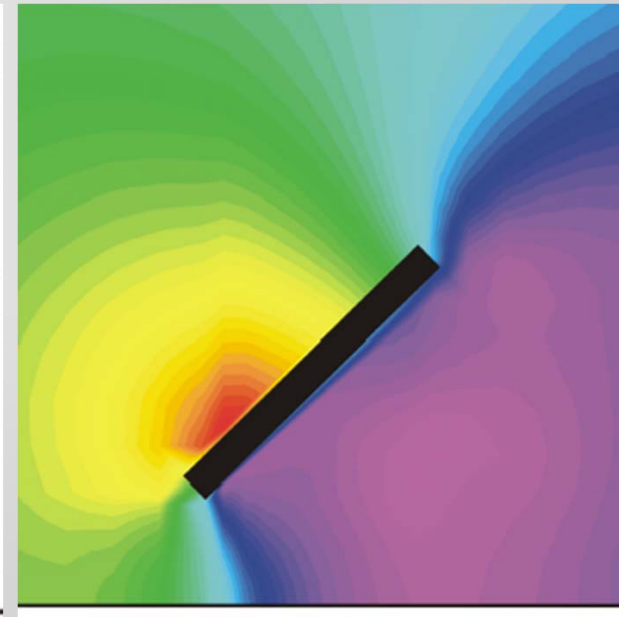
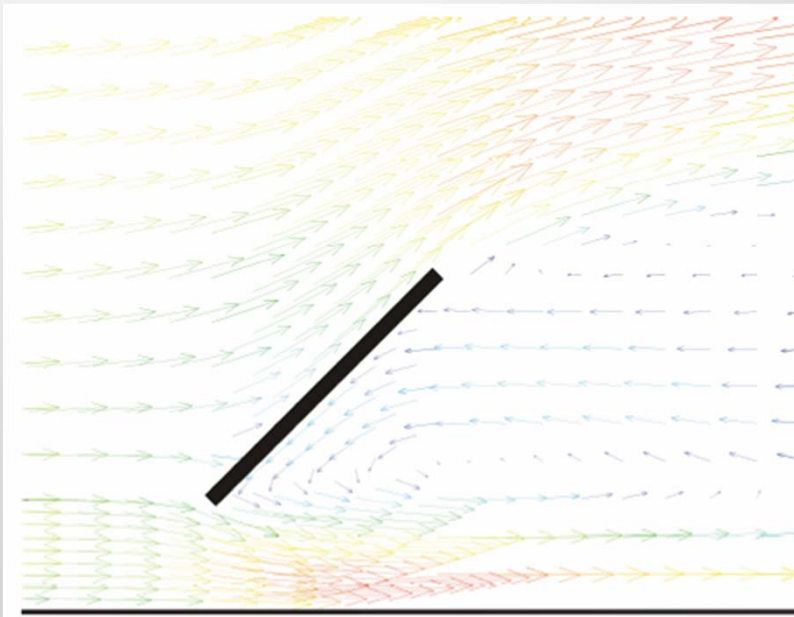
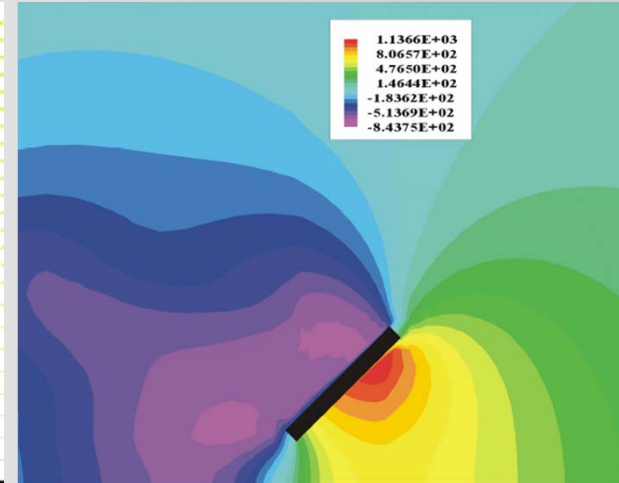
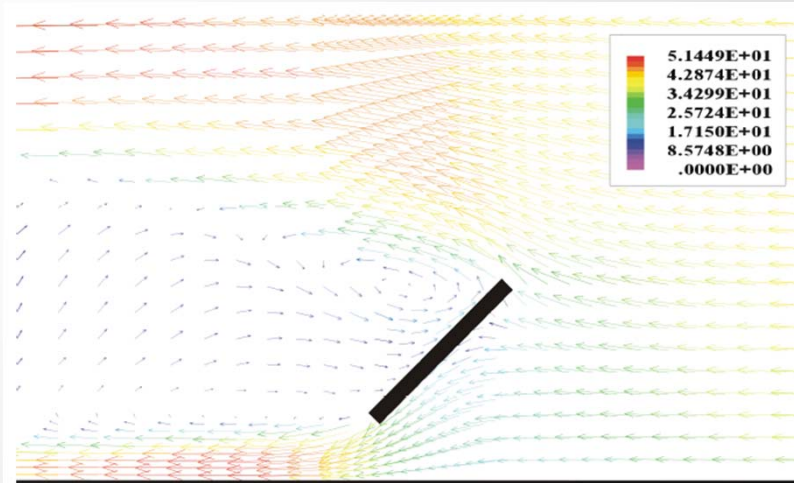
Source: Final report 0327229 A, patronized by the Federal Ministry of Economy and Technology

# Aerodynamic correlations


(45° inclination)

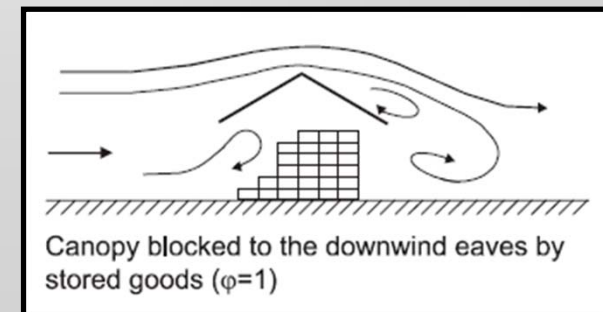
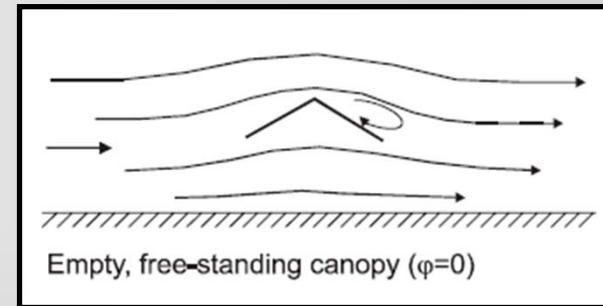
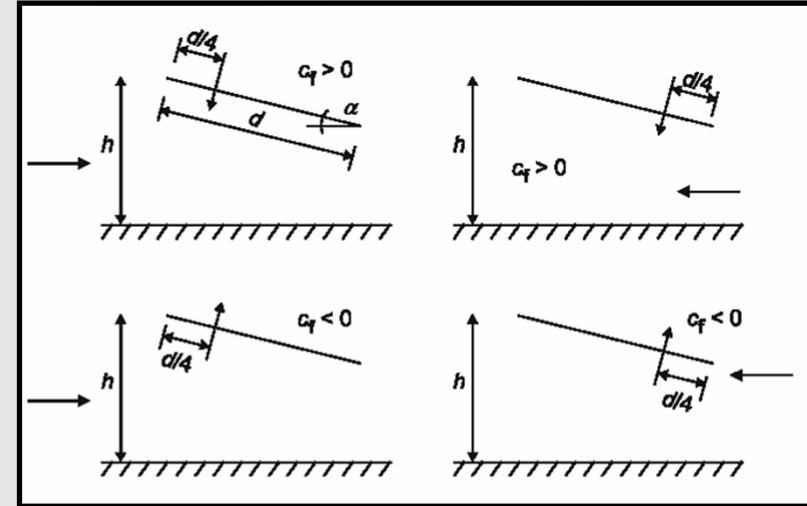


Wind direction



# Pressure and Force Coefficients (DIN EN 1991-1-4)

			Net Pressure coefficients $c_{p,net}$ Key plan		
Roof angle $\alpha$	Blockage $\varphi$	Overall Force Coefficients $c_r$	Zone A	Zone B	Zone C
0°	Maximum all $\varphi$	+ 0,2	+ 0,5	+ 1,8	+ 1,1
	Minimum $\varphi = 0$	- 0,5	- 0,6	- 1,3	- 1,4
	Minimum $\varphi = 1$	- 1,3	- 1,5	- 1,8	- 2,2
5°	Maximum all $\varphi$	+ 0,4	+ 0,8	+ 2,1	+ 1,3
	Minimum $\varphi = 0$	- 0,7	- 1,1	- 1,7	- 1,8
	Minimum $\varphi = 1$	- 1,4	- 1,6	- 2,2	- 2,5
10°	Maximum all $\varphi$	+ 0,5	+ 1,2	+ 2,4	+ 1,6
	Minimum $\varphi = 0$	- 0,9	- 1,5	- 2,0	- 2,1
	Minimum $\varphi = 1$	- 1,4	- 2,1	- 2,6	- 2,7
15°	Maximum all $\varphi$	+ 0,7	+ 1,4	+ 2,7	+ 1,8
	Minimum $\varphi = 0$	- 1,1	- 1,8	- 2,4	- 2,5
	Minimum $\varphi = 1$	- 1,4	- 1,6	- 2,9	- 3,0
20°	Maximum all $\varphi$	+ 0,8	+ 1,7	+ 2,9	+ 2,1
	Minimum $\varphi = 0$	- 1,3	- 2,2	- 2,8	- 2,9
	Minimum $\varphi = 1$	- 1,4	- 1,6	- 2,9	- 3,0
25°	Maximum all $\varphi$	+ 1,0	+ 2,0	+ 3,1	+ 2,3
	Minimum $\varphi = 0$	- 1,6	- 2,6	- 3,2	- 3,2
	Minimum $\varphi = 1$	- 1,4	- 1,5	- 2,5	- 2,8
30°	Maximum all $\varphi$	+ 1,2	+ 2,2	+ 3,2	+ 2,4
	Minimum $\varphi = 0$	- 1,8	- 3,0	- 3,8	- 3,6
	Minimum $\varphi = 1$	- 1,4	- 1,5	- 2,2	- 2,7

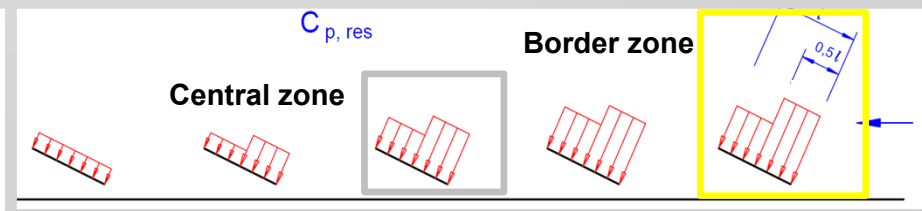
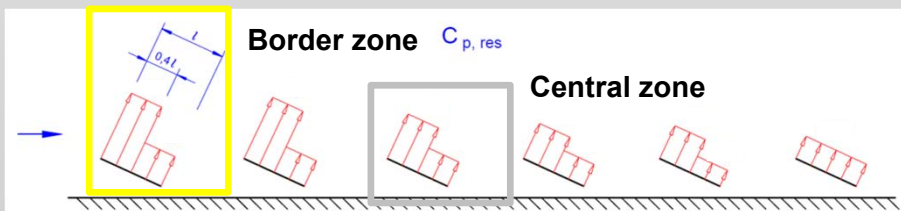
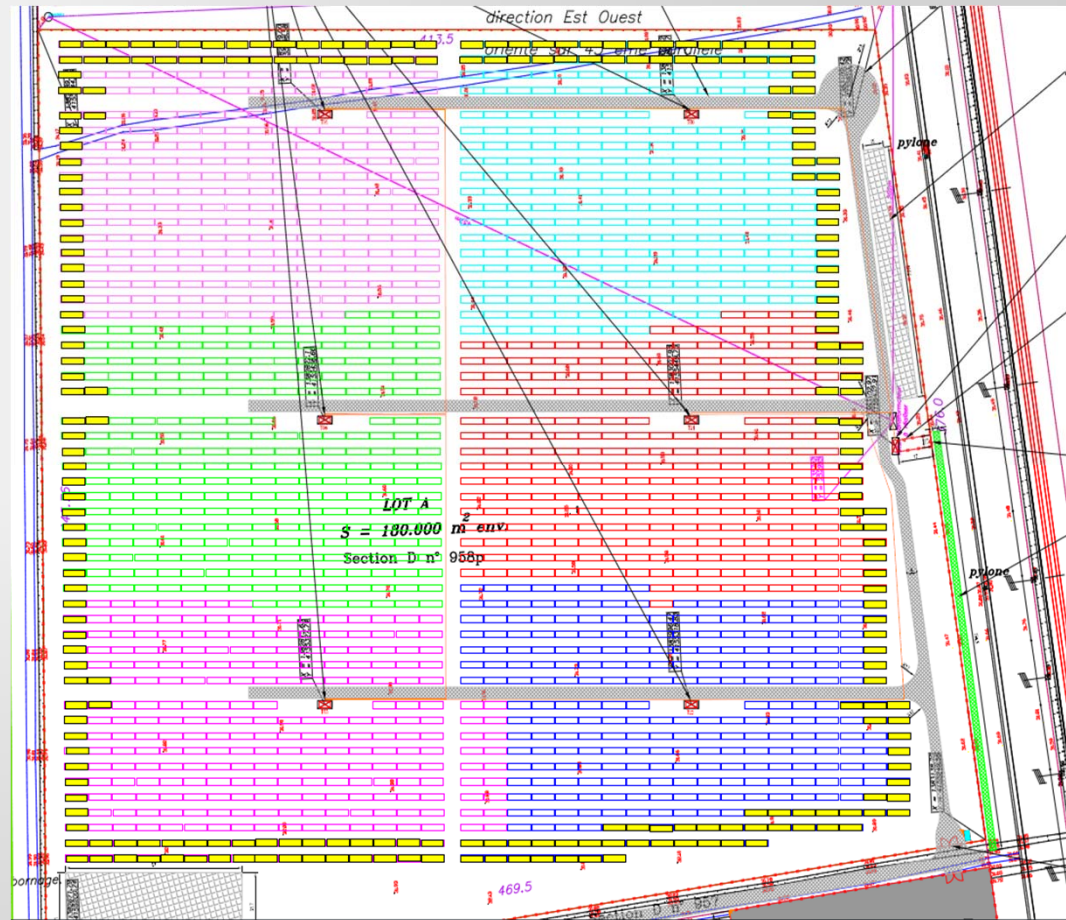
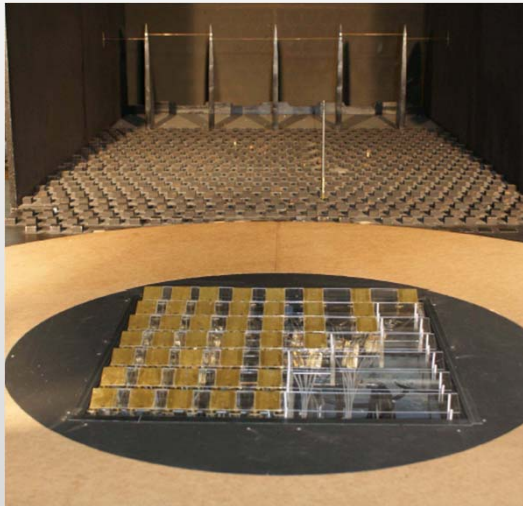


# Pressure Coefficients from Windtunnel tests

According to Ruscheweyh Consult GmbH

Advantages:

- Load reduction in central areas
- Savings (less posts)



# Increasing wind loads in case of isolated hills and ridges

$v_m$ : mean wind velocity at height  $z$  above terrain  
 $v_{mf}$ : mean wind velocity above flat terrain  
 $c_o = v_m/v_{mf}$

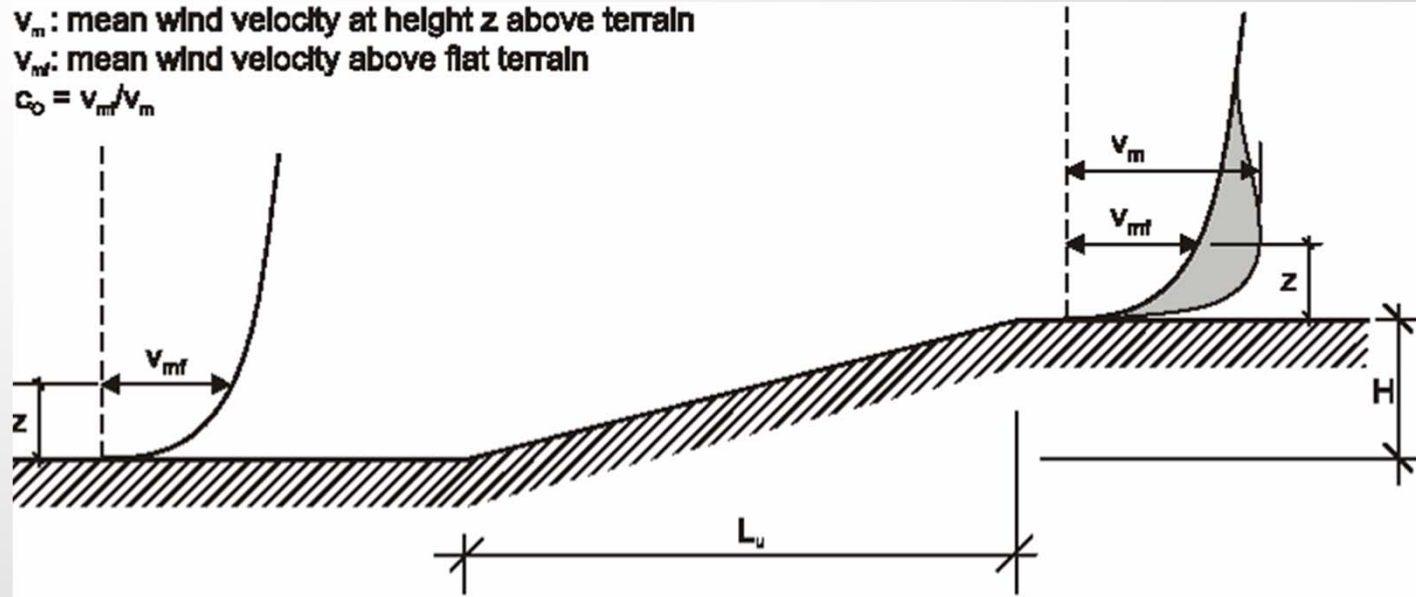


Figure A.1 — Illustration of increase of wind velocities over orography

**Increasing wind loads up to 42 % in case of changing topology (isolated hills and ridges)**



### 3. Design calculations for PV systems

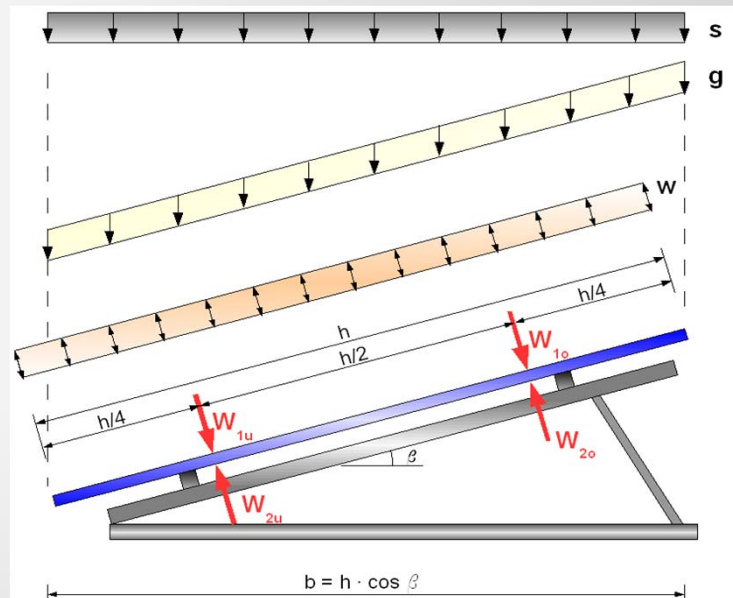
#### Load combinations

LC 1:  $1,35 \cdot g + 1,5 \cdot s + 0,6 \cdot 1,5 \cdot w$

LC 2:  $1,35 \cdot g + 0,5 \cdot 1,5 \cdot s + 1,5 \cdot w$

**LC 3:  $0,9 \cdot g + 1,5 \cdot w$**

(uplift)

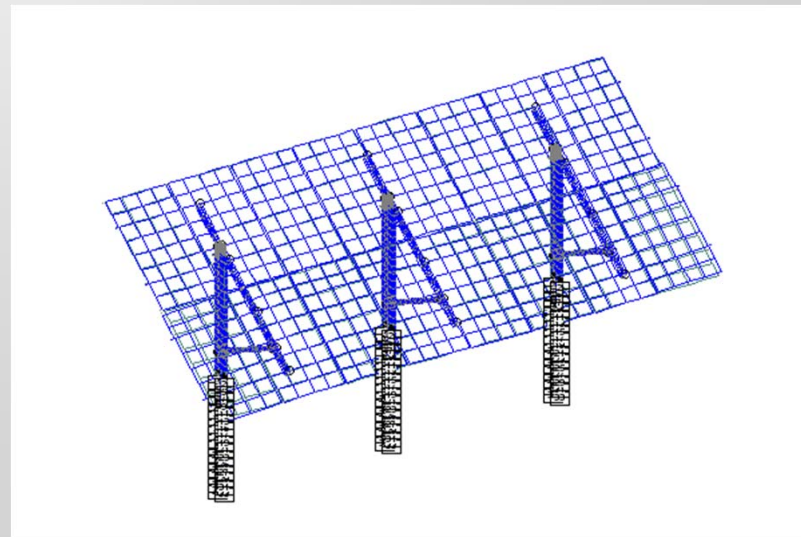
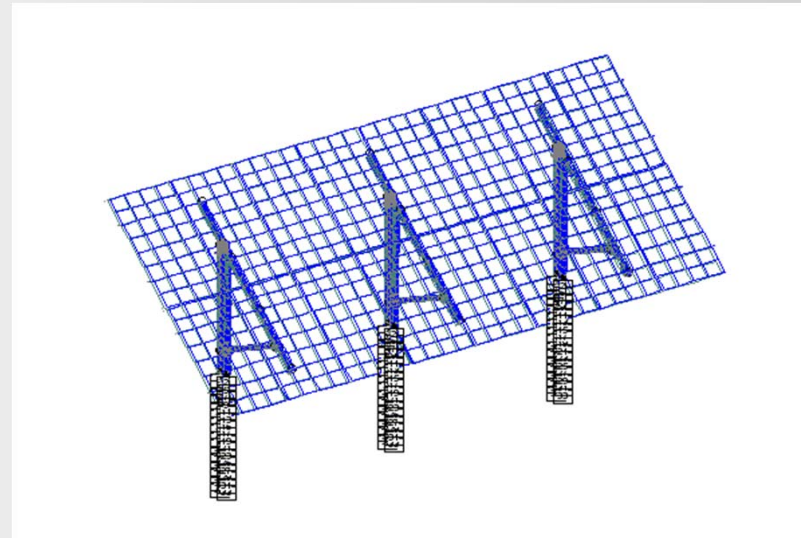


#### Verifications

- tilting
- dragging
- uplift



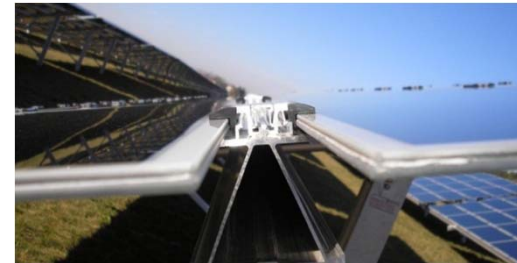
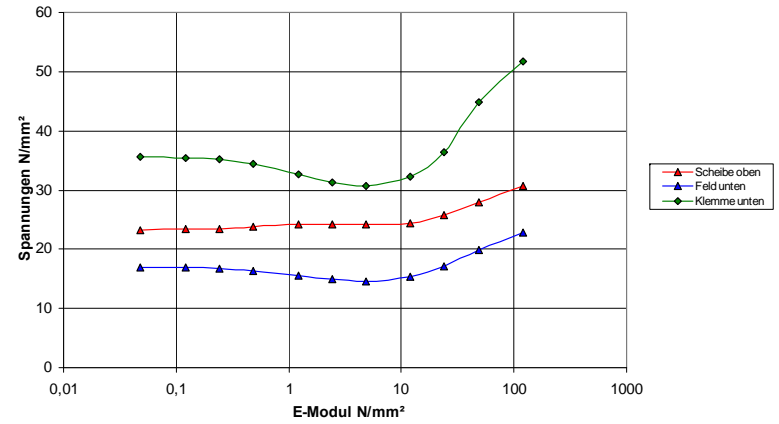
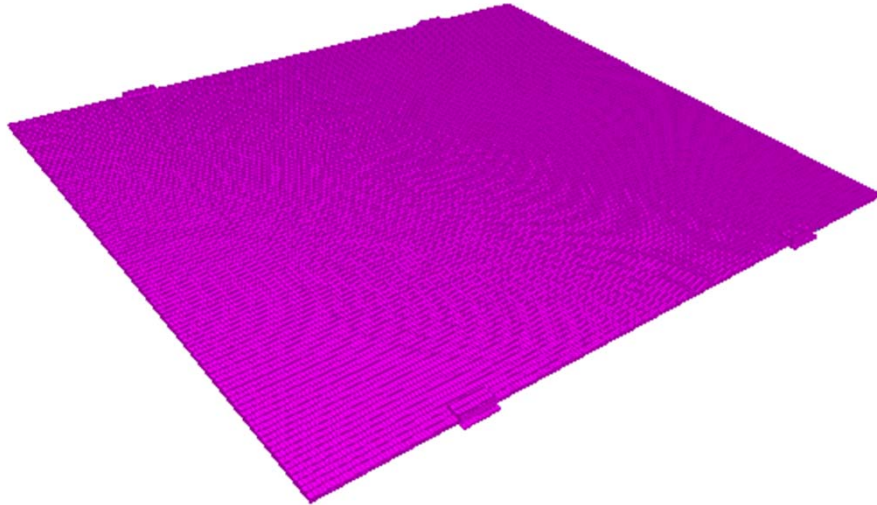
# Wind-induced vibrations / seismic design



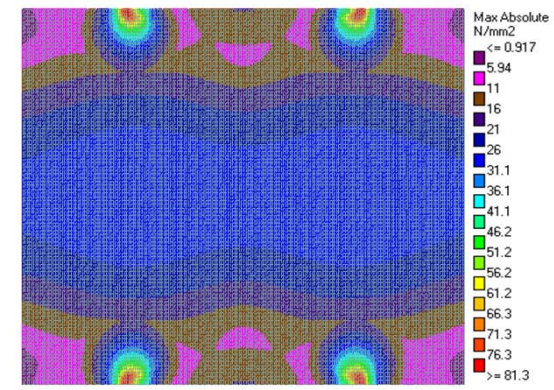
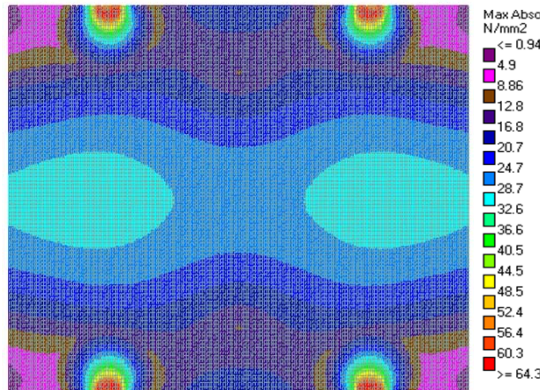
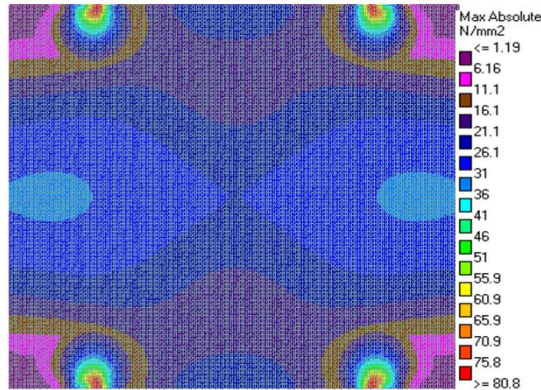


# Stress calculations for frameless modules

## Numerical model



## Stress calculations for thin-film modules



## 4. Decision criteria for substructure selection

**Material** (dimensioning acc. to basic material standards)

### Aluminum

- + low selfweight
- + shaping by extrusion process
- + easy to install (tolerance equalization)
- + remaining value
- floating material prices
- low young's modulus



### Steel

- + availability / well-proven solutions
- corrosion protection
- mounting effort
- high weight



### Timber

- + cost-saving for self-mounting
- durability
- contour accuracy

# 5. Foundation concepts for ground mounted Systems

## Pile-driven posts



- Pull-out capacity (vertical)
- Horizontal stiffness
- Bending moment in posts
- Drilling in case of rocks
- Chemical composition (corrosion)

## Screw foundations



- Pull-out capacity
- No horizontal stiffness
- Axial forces
- Drilling in case of rocks
- Chemical composition (corrosion)

## Concrete foundation

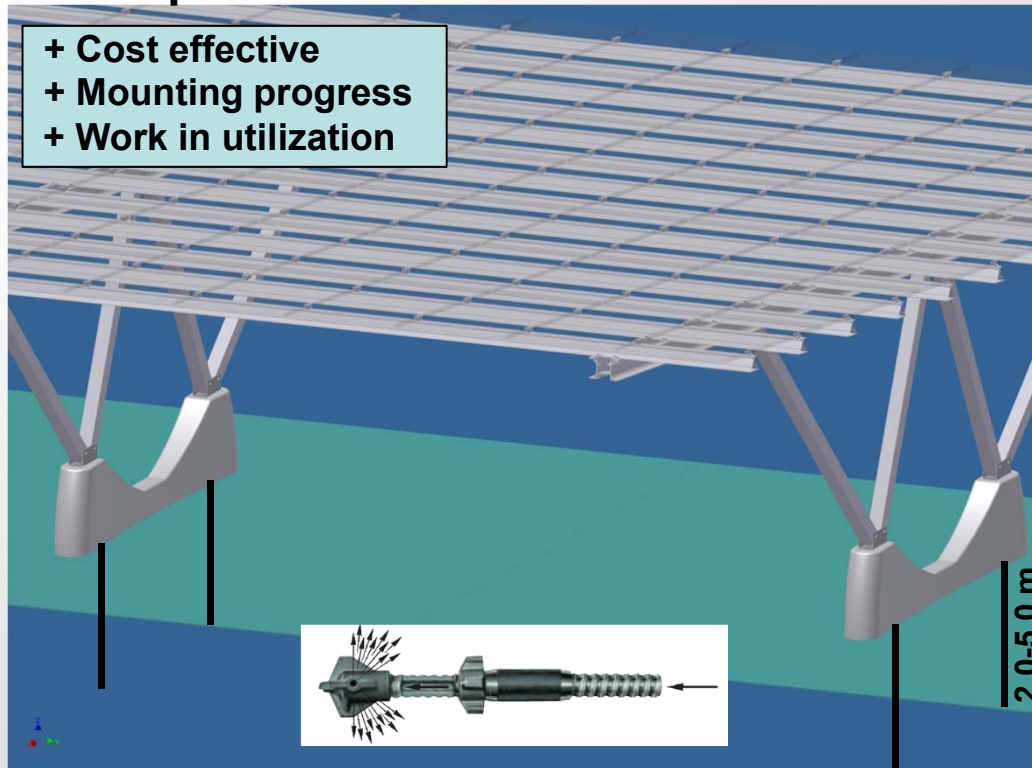


- Pressure stability of the soil
- Sensitivity of the top soil towards water
- Aggressive soil

# Foundation concepts for Carport Systems (Park@Sol)

## Micro piles

- + Cost effective
- + Mounting progress
- + Work in utilization



## Concrete foundations



- + Possible for most soil conditions
- Cost intensive (material)
- Mounting progress
- Damage of existing parking lots



# 6. Mounting progress of different foundation concepts

## Ground mounted Systems



**Ram-driven posts**

**1 MW/week**



**Concrete**

**1 MW/3 weeks  
(In situ concrete)**

**1 MW/2 weeks  
(precasted)**



## Carportsystem Park@Sol



**Micropiles**

**1 MW/2 weeks**

**excluding  
corrugated  
sheets**



**Concrete**

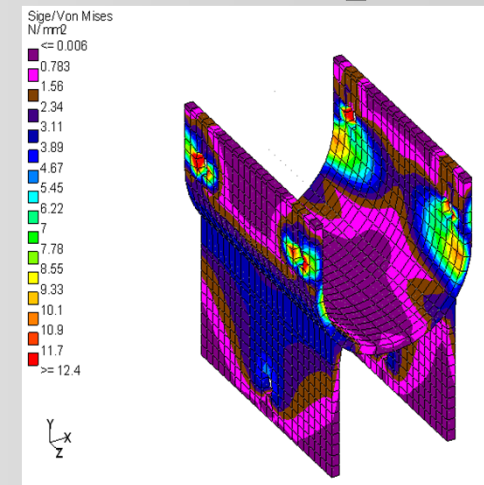
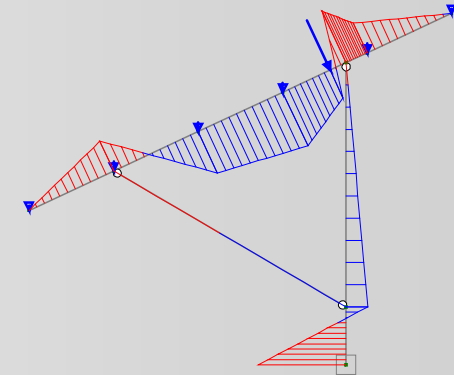
**1 MW/6 weeks**

**including  
corrugated  
sheets**



## 7. Conclusions

- Design calculations according to national standards
- Safety standards have to be verified for
  - Authorities
  - Insurance
  - Banking
- Target: Minimum BOS costs
  - Material cost
  - Mounting effort
  - Maintenance over life time
- Ram systems can be mounted significant faster
- The suitable system depends on soil conditions



**Thanks for your attention**

